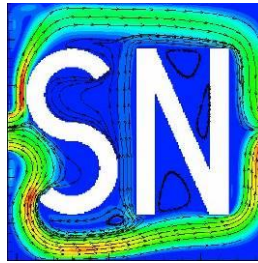
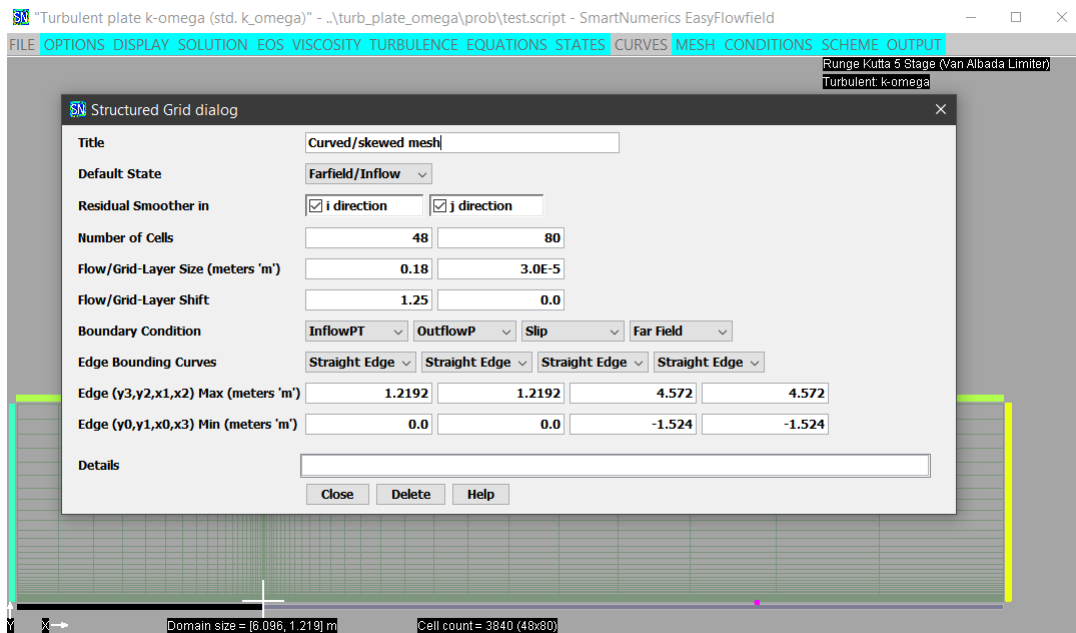


**Turbulent Flow Over Smooth Flat Plate**  
SmartNumerics Simulation Solutions Inc.



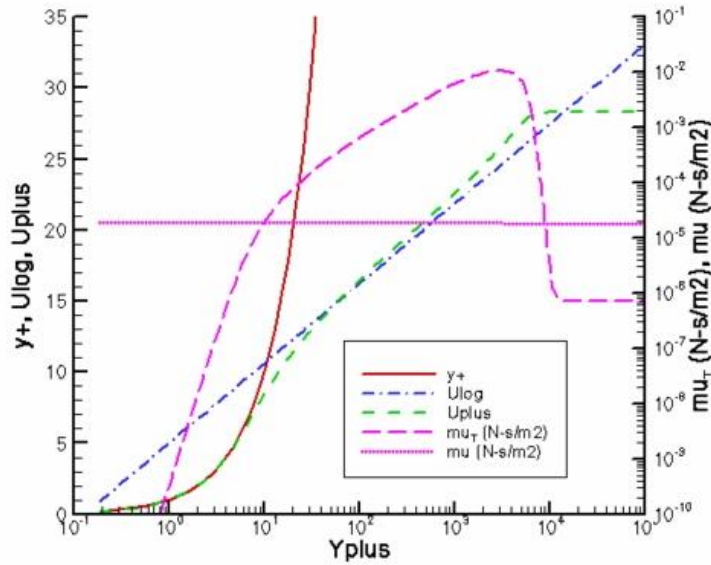
June 8, 2020

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**Fig. 1: Grid and  $k-\omega$  turbulence model input for turbulent flow over flat plate.**

Figure 1 displays the grid used to simulate turbulent flow of air over a flat plate using the ideal-gas equation of state. The  $k-\omega$  turbulence model of Wilcox [1] is used without a wall function. The far-field conditions are Mach 0.2, 101325 Pascals, and 300° K. The Sutherland formula is used to compute molecular viscosity.

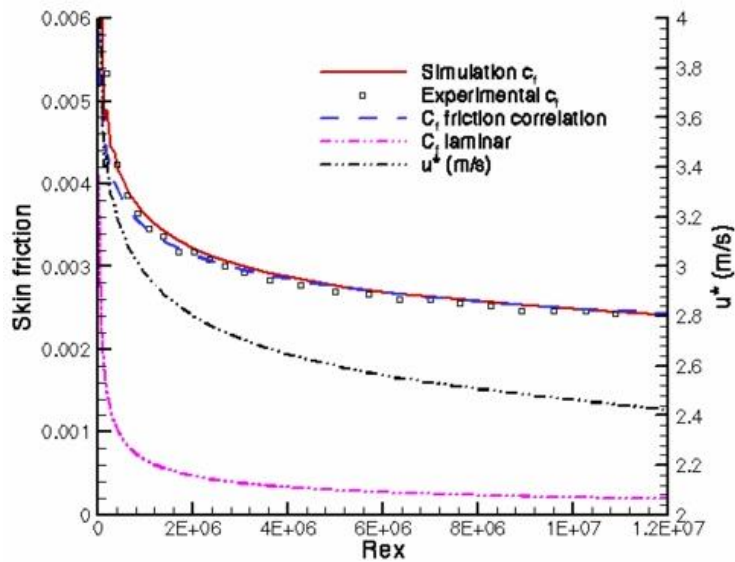


**Fig. 2: Plot of viscosity and  $u^+$  versus  $y^+$  for turbulent flow over smooth flat plate.**

Figure 2 displays a comparison of  $u^+ = u/u^*$  to the incompressible log law

$$U_{\log} = \frac{1}{0.41} \ln(y^+) + 5.0$$

at a region downstream of the leading edge. As expected, the  $u^+$  curve conforms to the  $y^+$  curve near the wall. Also shown is the variation of molecular velocity and eddy viscosity. The simulation was solved using an explicit five stage Runge-Kutta solver with enriched w-cycle multigrid. The HLLC flux was used with the van Albada limiter.



**Fig 3: Plot of skin friction vs Reynolds number for turbulent flow over smooth plate.**

Figure 3 displays the skin friction along the plate as a function of Reynolds number based on distance downstream from the leading edge. The skin friction velocity ( $u^*$ ) is also displayed. The skin friction coefficients are computed using

$$c_f = 2 \frac{\rho_w (u^*)^2}{\rho_\infty U_\infty^2}$$

using the local friction velocity output by the solver. Here,  $\rho_w$  is the local density at the wall,  $\rho_\infty$  is the far-field density, and  $U_\infty$  is the far-field velocity.

The friction obtained from the simulation is a good match to the fully turbulent friction correlation

$$c_{f \text{ fully turb}} = .025 (\text{Re}_x)^{-1/7}$$

as well as to experimental points taken from Wieghardt and Tillman [2]. The friction curve for turbulent flow is well above the Blasius friction correlation for laminar flow

$$c_{f \text{ laminar}} = \frac{0.664}{\sqrt{\text{Re}_x}}$$

Here

$$\text{Re}_x = \frac{\rho_\infty u_\infty x}{\mu_\infty}$$

is the Reynolds number a specified distance  $x$  downstream of the leading edge of the plate, where  $\mu_\infty$  is the far-field molecular viscosity,  $u_\infty$  is the far-field velocity, and  $\rho_\infty$  is the far-field density.

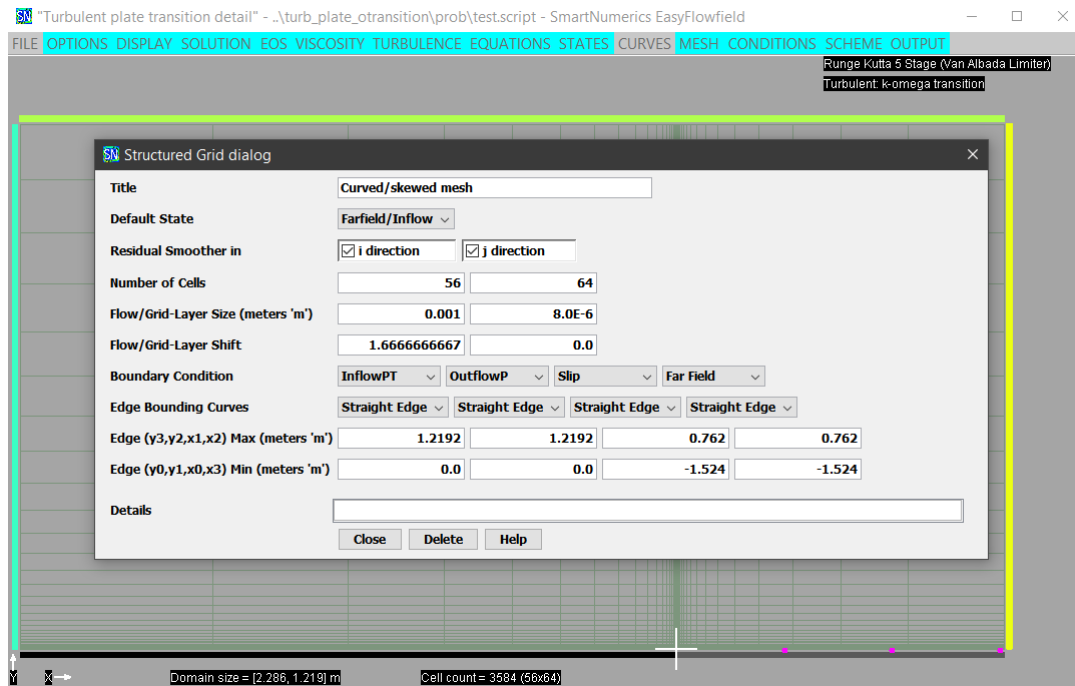
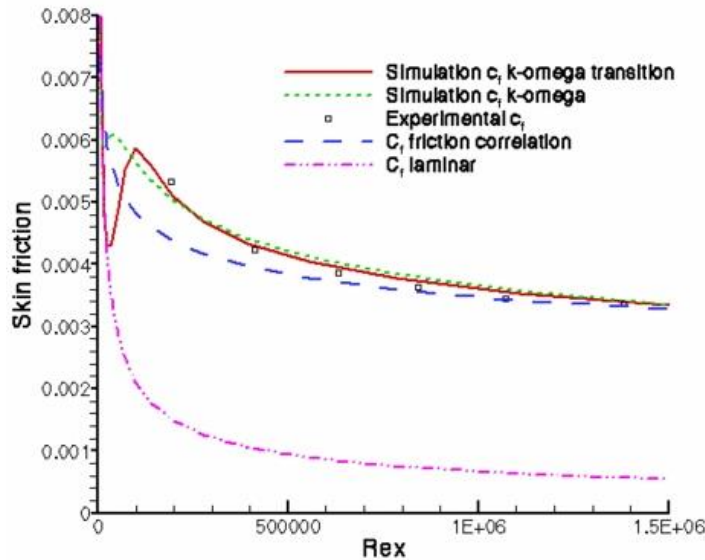


Fig. 4: Grid used for simulation of turbulent flow over plate at lower  $\text{Re}_x$ .



**Fig 5: Plot of skin friction vs Reynolds number for turbulent flow over smooth plate.**

All but one of the turbulence models currently implemented in EasyFlowfield assume fully turbulent flow and produce a friction curve similar to that produced by the  $k-\omega$  model. The  $k-\omega$  transition turbulence model of Wilcox [1] is tuned to model transition from laminar to turbulent flow near the leading edge of a smooth flat plate. As seen in Figure 5, the friction computed using the  $k-\omega$  transition turbulence model on a shortened plate follows the laminar friction curve up to a certain point then moves upward as flow becomes turbulent further downstream. The friction computed using the  $k-\omega$  turbulence model does not match the laminar friction curve. As one might expect, the fully turbulent friction correlation lies well under the experimental points until the Reynolds number exceeds 800,000.

## References

- [1] Wilcox, D. C., Turbulence Modeling for CFD, DCW Industries Inc., 1994.
- [2] Wieghardt, K. and Tillman, W., On the Turbulent Friction Layer for Rising Pressure, NACA TM-1314, 1951.